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EMBEDDED ATOMS IN A CRYSTALLINE HEXAGONAL STRUCTURE

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As part of the work, the hexagonal structure of B19 type metals as hydrogen sorbents will be considered. That is, crystal lattices are considered, where atoms of impurities (hydrogen) are introduced into the interstices of the metal. To do this, we present an image of the B19 structure itself. In this work, the solubility of hydrogen in the crystal structure of B19 type metals was studied using the configuration method, and the dependence on the composition of the alloy and temperature was found in the substitution of nodes and interstices. Also, in the work the degrees of long-range order at the nodes are considered and the parameters of the correlation in the substitution are determined. A graphical view of the effect of atomic order on the solubility of impurities is given. The calculated data obtained in the work coincide with the experimental data of other studies, and the obtained calculation formulas make it possible to determine the energy parameters of the alloys, which is a certain scientific value of the work. The proposed system takes into account only atomic interaction and absorption (dissolution) and diffusion of interstitial atoms into the bulk of the crystal structure; therefore, it is possible to predict the introduction of only a hydrogen atom. Thus, the results obtained in the work of the correlation parameters for the distribution of atoms only in octapores or only in tetrapores allow a deeper study of the physical characteristics of alloys of the B19 type and an understanding of the processes of hydrogen sorption by the working bodies of hydrogen storage.

Keywords: Hydrogen, metal, alloys, solubility, introduction impurities, correlation parameters, substitution impurities, B19 structure

INTRODUCTION

Today, the study of the solubility of impurities introduced into the metal crystal structure is mostly based on the results of research on the production of metals [1–4], alloys [5–7], and their mechanical mixtures [8–10]. Such materials can play the role of catalysts [11–24] for the synthesis of a number of nanostructures (fullerenes [25–28], fullerites [29], endofullerenes [30], nanotubes [31–34] and others [35–39]) in various methods of synthesis [40–46]. All catalysts and related synthesized nanostructures allow to compete with other micro [47–79] and nanofillers [50–58] for modern composites that have more or less a range of applications in various fields: solar panels [59–61], additive technologies [62–65], sorption

fields [66–72], biological and medical fields [73–77], as well as in hydrogen energy [78–100].

In the field of hydrogen energy, materials that can serve as hydrogen sorbents [78–100] are of special scientific and practical interest to solve the problem of storing and transporting hydrogen as a power source of the energy “hydrogen cycle”. Both carbon nanostructures [78–82] and metals [83–86] and their alloys [87–100] are being studied to create hydrogen sorbents.

SOLUBILITY, IMPURITIES, IMPLEMENTATION

The solubility of the introduced impurity was studied mainly for alloys with different structures [101, 102], the correlation in the substitution of nodes and internodes – for disordered alloys [103]. In this work, we consider a metal with a

hexagonal structure B19, into the interstices of which insertion atoms are introduced, let's call them C-atoms. The B19 structure has two types of octahedral O_1 , O_2 and one type of tetrahedral T internodes. Fig. 1 shows the studied structure in

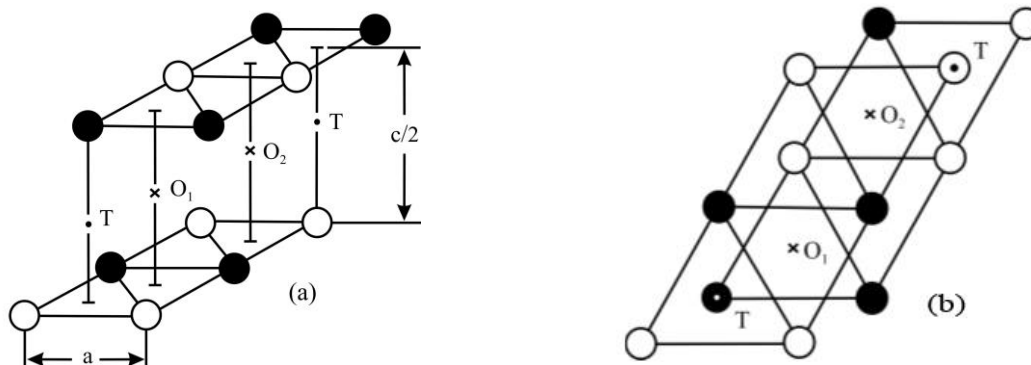


Fig. 1. Image of the hexagonal structure of B19. *a* – spatial image of the B19 structure; *b* – projection image of the B19 structure along the C axis. Black circles (●) show nodes of the first type, legal for A atoms; light circles (○) show nodes of the second type, legal for B atoms; crosses (×) – octapores; dots (•) – tetrapores

To determine the solubility and correlation properties, it is necessary to calculate the free energy of metal F. We use the method of configurations, that is, we take into account all kinds of changes of atoms A for each internode. The configuration is

$$\begin{aligned}
 F = & \sum_{l=0}^6 (N_{O_1}^l + N_{O_2}^l) \nu_l - \sum_{l=0}^4 N_T^l \nu'_l - \kappa \Theta \left[\sum_{l=0}^6 Q_{O_1}^l \ln Q_{O_1}^l + \sum_{l=0}^6 Q_{O_2}^l \ln Q_{O_2}^l + \sum_{l=0}^4 Q_T^l \ln Q_T^l - \right. \\
 & - \sum_{l=0}^6 N_{O_1}^l \ln N_{O_1}^l - \sum_{l=0}^6 N_{O_2}^l \ln N_{O_2}^l - \sum_{l=0}^4 N_T^l \ln N_T^l - \sum_{l=0}^6 (Q_{O_1}^l - N_{O_1}^l) \ln (Q_{O_1}^l - N_{O_1}^l) - \\
 & \left. - \sum_{l=0}^6 (Q_{O_2}^l - N_{O_2}^l) \ln (Q_{O_2}^l - N_{O_2}^l) - \sum_{l=0}^4 (Q_T^l - N_T^l) \ln (Q_T^l - N_T^l) \right], \quad (1)
 \end{aligned}$$

where $N_{O_1}^l$, $N_{O_2}^l$, N_T^l is the number of C atoms in pores O_1 , O_2 , T; $Q_{O_1}^l$, $Q_{O_2}^l$, Q_T^l – the number of these pores in the alloy; $\nu_l = l \alpha + (6-l) \beta$ $\nu'_l = l \alpha' + (4-l) \beta'$ – energies of the C atom in octa- and tetrapores; $\alpha = \nu_{AC}$, $\beta = \nu_{BC}$ – $\alpha' = \nu'_{AC}$, $\beta' = \nu'_{BC}$ energy of interaction of the nearest pairs of the specified atoms; k – Boltzmann's constant; Θ – absolute temperature.

From the conditions of minimum free energy, we find the numbers

spatial (Fig. 1 *a*) and projection along the C axis (Fig. 1 *b*) images. Black circles show nodes of the first type, legal for A atoms; light circles show nodes of the second type, legal for B atoms; crosses – octapores; points – tetrapores.

denoted by the index l , which determines the number of nearest atoms around the pore. The free energy can be presented in the form specified in formula (1) [102, 103].

$$\begin{aligned}
 N_{O_1}^l &= \frac{D Q_{O_1}^l \exp \frac{\nu_l}{\kappa \Theta}}{1 + D Q_{O_1}^l \exp \frac{\nu_l}{\kappa \Theta}}; \quad N_{O_2}^l = \frac{D Q_{O_2}^l \exp \frac{\nu_l}{\kappa \Theta}}{1 + D Q_{O_2}^l \exp \frac{\nu_l}{\kappa \Theta}}; \\
 N_T^l &= \frac{D Q_T^l \exp \frac{\nu'_l}{\kappa \Theta}}{1 + D Q_T^l \exp \frac{\nu'_l}{\kappa \Theta}}, \quad (2)
 \end{aligned}$$

which are connected by an obvious ratio

$$\sum_{l=0}^6 (N_{O_1}^l + N_{O_2}^l) + \sum_{l=0}^4 N_T^l = N_C, \quad (3)$$

where N_C is the number of all C atoms in the alloy. The coefficient D included in formulas (2) is a multiplier by which the state function of the system increases when each additional atom appears in it in the process of dissolving impurities. When studying the correlation, if we count $N_C = \text{const}$, the coefficient D is determined

$$N_o = N \left(1 + \frac{1}{D} \exp \frac{-6\alpha}{\kappa\Theta} \right)^{-1}; \quad N_T = 2N \left(1 + \frac{1}{D} \exp \frac{-4\alpha'}{\kappa\Theta} \right)^{-1}, \quad (4)$$

summing up them we find the solubility of the component

$$v = \frac{N_o + N_T}{3N} = \frac{1}{3} \left[\left(1 + \frac{1}{D} \exp \frac{-6\alpha}{\kappa\Theta} \right)^{-1} + 2 \left(1 + \frac{1}{D} \exp \frac{-4\alpha'}{\kappa\Theta} \right)^{-1} \right]. \quad (5)$$

If C atoms are located only in octapores or only in tetrapores, then the solubilities should be determined according to the formulas:

$$v_o = \frac{N_o}{N} = \left(1 + \frac{1}{D} \exp \frac{-6\alpha}{\kappa\Theta} \right)^{-1}; \quad v_T = \frac{N_T}{2N} = \left(1 + \frac{1}{D} \exp \frac{-4\alpha'}{\kappa\Theta} \right)^{-1}. \quad (6)$$

In the case of low concentrations of the component, these ratios are simplified

$$v_o = D \exp \frac{6\alpha}{\kappa\Theta}; \quad v_T = D \exp \frac{4\alpha'}{\kappa\Theta}, \quad (7)$$

that is, a linear dependence of the natural logarithm of the solubility of the introduced atoms on the inverse temperature is manifested. The dependences of $\ln v_o$ and $\ln v_T$ from $1/\Theta$ (6) are not linear, but monotonic.

If the solubility is described by formula (5), then it is possible to manifest its extreme properties in the temperature dependence at

$$\frac{\alpha}{\alpha'} = -\exp \frac{2(3\alpha - 2\alpha')}{\kappa\Theta}; \quad (8)$$

at the same time, the energy parameters α and α' must have different signs. In this case, the distribution of C atoms in the octa- and tetrapores is uneven. It can be estimated from the equations

$$v_o + 2v_T = 3c; \quad \frac{v_o(1-v_T)}{v_T(1-v_o)} = \exp \frac{2(3\alpha - 2\alpha')}{\kappa\Theta}, \quad (9)$$

from condition (3). Formulas (2) are valid for any numbers of filling of internodes with C atoms.

In the particular case of metal A, when $l = 6$, $v_l = 6\alpha$, $Q_o = N$ for octapores and $l = 4$, $v_l' = 4\alpha'$, $Q_T = 2N$ for tetrapores (N is the number of alloy nodes), instead of nineteen formulas (2) we have two

where $c = N_C/3N$. The first is obtained from system (4) by excluding the multiplier D , the second is condition (3).

Solving system (9), we find

$$v_o = \frac{3c(1-\varepsilon) - 2 - \varepsilon + \sqrt{[3c(1-\varepsilon) - 2 - \varepsilon]^2 + 12c\varepsilon(1-\varepsilon)}}{2(1-\varepsilon)},$$

$$v_T = \frac{3}{2}c - \frac{1}{2}v_o. \quad (10)$$

where $\varepsilon = \exp \frac{2(3\alpha - 2\alpha')}{\kappa\Theta}$ is marked. When $c = 1$, distribution (10) gives $v_o = v_T = 1$, that is, we have uniform filling of all internodes regardless of temperature.

At low temperatures, the distribution of atoms is determined by the ratio of energy parameters α and α' . If $3\alpha - 2\alpha' > 0$, at absolute zero of temperature we have

$$v_o(0) = \begin{cases} 3c \text{ at } 0 \leq c \leq \frac{1}{3} \\ \frac{1}{3} \text{ at } \frac{1}{3} \leq c \leq 1, \end{cases} \quad v_T(0) =$$

$$= \begin{cases} 0 & \text{at } 0 \leq c \leq \frac{1}{3} \\ \frac{3}{2}c - \frac{1}{2} & \text{at } \frac{1}{3} \leq c \leq 1, \end{cases} \quad (11)$$

that is, the introducing atoms first occupy the octapores, in which they have a deeper potential energy minimum, and only when the octapores are occupied do the tetrapores begin to fill. If $3\alpha - 2\alpha' < 0$, then

$$v_O(0) = \begin{cases} 0 & \text{at } 0 \leq c \leq \frac{2}{3} \\ 3c - 2 & \text{at } \frac{2}{3} \leq c \leq 1, \end{cases} \quad v_T(0) =$$

$$= \begin{cases} \frac{3}{2}c & \text{at } 0 \leq c \leq \frac{2}{3} \\ 1 & \text{at } \frac{2}{3} \leq c \leq 1, \end{cases} \quad (12)$$

that is, first of all, C atoms fill the tetrapores. Dependences (11) and (12) are represented by straight lines in Fig. 2. Curved lines in this figure show the dependences of $v_O(0)$ and $v_T(0)$, constructed according to distribution (10) at the temperatures Θ_1 and Θ_2 .

$$\Theta_1 = \frac{4(1,5\alpha - \alpha')}{\kappa \ln 10} \quad (a) \quad \text{and}$$

$$\Theta_2 = -\frac{4(1,5\alpha - \alpha')}{\kappa \ln 10} \quad (b)$$

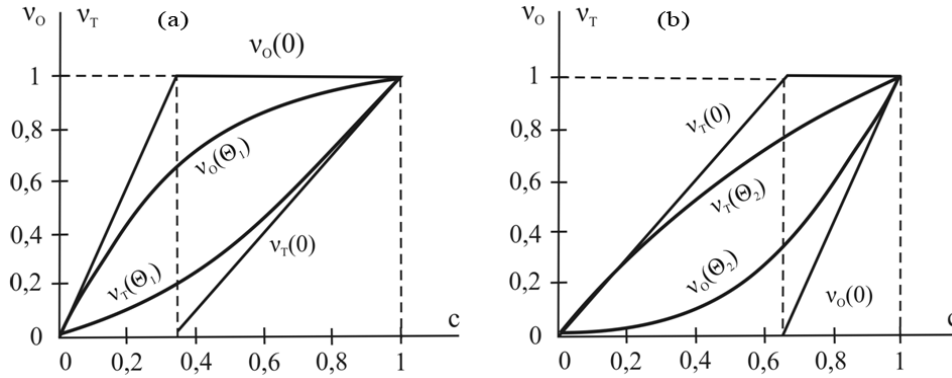


Fig. 2. Graphic representation of dependences (11), (12), and $v_O(0)$ and $v_T(0)$ according to distribution (10) at the temperatures Θ_1 (a) and Θ_2 (b)

It is necessary to consider the second special case - a binary alloy with a low concentration of the introduction impurity. In this case, relation (2) is simplified:

$$N_{O_1}^l = DQ_{O_1}^l \exp \frac{v_l}{\kappa\Theta}; \quad N_{O_2}^l = DQ_{O_2}^l \exp \frac{v_l}{\kappa\Theta}; \quad N_T^l = DQ_T^l \exp \frac{v_l'}{\kappa\Theta}, \quad (13)$$

and $Q_{O_1}^l, Q_{O_2}^l, Q_T^l$ numbers are determined by the configuration of A atoms around voids

$$Q_{O_1}^l = \frac{1}{2} N \frac{4!}{i!(4-i)!} p_A^{(1)i} p_B^{(1)(4-i)} \cdot \frac{2!}{j!(2-j)!} p_A^{(2)j} p_B^{(2)(2-j)}$$

$$Q_{O_2}^l = \frac{1}{2} N \frac{2!}{i!(2-i)!} p_A^{(1)i} p_B^{(1)(2-i)} \cdot \frac{4!}{j(4-j)!} p_A^{(2)j} p_B^{(2)(4-j)}$$

$$Q_T^l = 2N \frac{2!}{i!(2-i)!} p_A^{(1)i} p_B^{(1)(2-i)} \cdot \frac{2!}{j!(2-j)!} p_A^{(2)j} p_B^{(2)(2-j)} \quad (14)$$

Here $l = i + j$, where i and j are the numbers of A atoms around the internode, respectively, on nodes of the first and second type, and $p_A^{(1)}, p_A^{(2)}, p_B^{(1)}, p_B^{(2)}$ are the probabilities of replacing nodes 1, 2 by atoms A, B, which depend on the composition a, b of the binary alloy and the degree of long-range order η according to the formulas [104]:

$$p_A^{(1)} = a + \frac{1}{2}\eta; \quad p_A^{(2)} = a - \frac{1}{2}\eta; \quad p_B^{(1)} = b - \frac{1}{2}\eta;$$

$$p_B^{(2)} = b + \frac{1}{2}\eta. \quad (15)$$

Summing up for all configurations of the quantity (13) taking into account (14), we obtain the numbers of C atoms in the pores O_1, O_2, T :

$$N_C^{O_1} = \frac{1}{2}NDK_1^4K_2^2; N_C^{O_2} = \frac{1}{2}NDK_1^2K_2^4, N_C^{(T)} = 2NDK_1'^2K_2'^2 \quad (16)$$

where

$$\begin{aligned} K_1 &= p_A^{(1)} \exp \frac{\alpha}{\kappa\Theta} + p_B^{(1)} \exp \frac{\beta}{\kappa\Theta}; \\ K_2 &= p_A^{(2)} \exp \frac{\alpha}{\kappa\Theta} + p_B^{(2)} \exp \frac{\beta}{\kappa\Theta}; \\ K_1' &= p_A^{(2)} \exp \frac{\alpha'}{\kappa\Theta} + p_B^{(1)} \exp \frac{\beta'}{\kappa\Theta}; \\ K_2' &= p_A^{(2)} \exp \frac{\alpha'}{\kappa\Theta} + p_B^{(2)} \exp \frac{\beta'}{\kappa\Theta}. \end{aligned} \quad (17)$$

The solubility of impurities, which is determined by the concentration of C atoms for each type of internodes, is obtained from (16)

$$\begin{aligned} v_o &= \frac{N_C^{(O_1)} + N_C^{(O_2)}}{N} = \frac{1}{2}DK_1^2K_2^2(K_1^2 + K_2^2), \\ v_T &= \frac{N_C^{(T)}}{2N} = DK_1'^2K_2'^2. \end{aligned} \quad (18)$$

These formulas together with (17) and (15) determine the dependence of solubility on alloy composition, temperature, and order parameters. The first dependence for a disordered alloy ($\eta = 0$) turns out to be monotonic, the second at $\eta = 0$ can be extreme, if

$$\frac{\alpha}{\beta} = -\frac{b}{a} \exp \frac{\beta - \alpha}{\kappa\Theta}$$

for the octa pores and

$$\frac{\alpha'}{\beta'} = -\frac{b}{a} \exp \frac{\beta' - \alpha'}{\kappa\Theta}$$

for tetrapores (in this case, the energy parameters α, β and α', β' must have different signs). The influence of atomic order on solubility is convenient to find out for relative values (Fig. 3).

$$\begin{aligned} f_o &= v_o / (v_o)_{\eta=0} = (1 - \chi_1^2)(1 - \chi_1^4), \\ f_T &= v_T / (v_T)_{\eta=0} = (1 - \chi_2^2)^2, \end{aligned} \quad (19)$$

where

$$\begin{aligned} \chi_1 &= \frac{1}{2} \eta \frac{\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta}}{a \exp \frac{\alpha}{\kappa\Theta} + b \exp \frac{\beta}{\kappa\Theta}}; \\ \chi_2 &= \frac{1}{2} \eta \frac{\exp \frac{\alpha'}{\kappa\Theta} - \exp \frac{\beta'}{\kappa\Theta}}{a \exp \frac{\alpha'}{\kappa\Theta} + b \exp \frac{\beta'}{\kappa\Theta}}; \\ -1 &\leq \chi_1, \chi_2 < 1. \end{aligned} \quad (20)$$

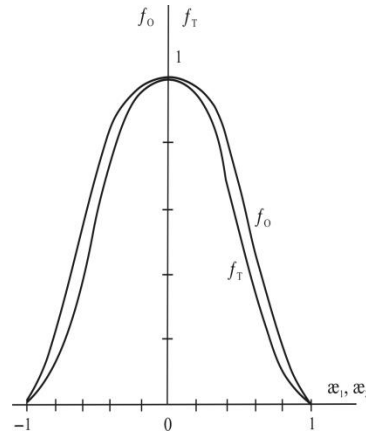


Fig. 3. Influence of atomic order on solubility

The nature of the dependence of the values f_o, f_T on η is the same. Ordering reduces solubility, for octapores this reduction is somewhat weaker.

In the case of distribution of the introduction impurity simultaneously on all internodes, the solubility is determined by the formula

$$\begin{aligned} v &= \frac{N_C^{(O_1)} + N_C^{(O_2)} + N_C^{(T)}}{3N} = \\ &= \frac{1}{6}D \left[K_1^2K_2^2(K_1^2 + K_2^2) + 4K_1'^2K_2'^2 \right]. \end{aligned} \quad (21)$$

The dependence of solubility on the composition at $\eta = 0$ can be extreme if the energies α and β or α' and β' are of different signs.

The nature of the dependence of v on η is the same as for the values v_O and v_T .

Let's find the correlation parameters in the substitution of nodes and internodes, counting $N_C = \text{const}$. From condition (3) taking into account (13), we find the coefficient D

$$D = 6c[K_1^2 K_2^2 (K_1^2 + K_2^2) + 4K_1'^2 K_2'^2]^{-1}. \quad (22)$$

$$\begin{aligned} N_{O_1}^i &= \sum_{j=0}^2 N_{O_1}^j = \frac{1}{2} DNK_2^2 \frac{4!}{i!(4-i)!} p_A^{(1)i} p_B^{(1)(4-i)} \exp \frac{i\alpha + (4-i)\beta}{\kappa\Theta}; \\ N_{O_1}^j &= \sum_{i=0}^4 N_{O_1}^i = \frac{1}{2} DNK_1^4 \frac{2!}{j!(2-j)!} p_A^{(2)j} p_B^{(2)(2-j)} \exp \frac{j\alpha + (2-j)\beta}{\kappa\Theta}; \\ N_{O_2}^i &= \sum_{j=0}^4 N_{O_2}^j = \frac{1}{2} DNK_2^4 \frac{2!}{i!(2-i)!} p_A^{(1)j} p_B^{(1)(2-i)} \exp \frac{i\alpha + (2-i)\beta}{\kappa\Theta}; \\ N_{O_2}^j &= \sum_{i=0}^2 N_{O_2}^i = \frac{1}{2} DNK_1^2 \frac{4!}{j!(4-j)!} p_A^{(2)j} p_B^{(2)(4-j)} \exp \frac{j\alpha + (4-j)\beta}{\kappa\Theta}; \\ N_T^i &= \sum_{j=0}^2 N_T^j = 2DNK_2'^2 \frac{2!}{i!(2-j)!} p_A^{(1)i} p_B^{(1)(2-i)} \exp \frac{i\alpha' + (2-i)\beta'}{\kappa\Theta}; \\ N_T^j &= \sum_{i=0}^2 N_T^i = 2DNK_1'^2 \frac{2!}{j!(2-j)!} p_A^{(2)j} p_B^{(2)(2-j)} \exp \frac{j\alpha' + (2-j)\beta'}{\kappa\Theta}. \end{aligned} \quad (23)$$

The posteriori and a priori probabilities of replacement of the nearest pairs of nodes and pores by atoms A, C are equal, respectively

$$\begin{aligned} p_{AC}^{(1O_1)} &= \frac{1}{2N} \sum_{i=0}^4 iN_{O_1}^i = DK_1^3 K_2^2 p_A^{(1)} \exp \frac{\alpha}{\kappa\Theta}; & p_{AC}^{(1O_1)^0} &= 2p_A^{(1)} N_C^{(O_1)} / N = DK_1^4 K_2^2 p_A^{(1)}; \\ p_{AC}^{(2O_1)} &= \frac{1}{N} \sum_{j=0}^2 jN_{O_1}^j = DK_1^4 K_2 p_A^{(2)} \exp \frac{\alpha}{\kappa\Theta}; & p_{AC}^{(2O_1)^0} &= 2p_A^{(2)} N_C^{(O_1)} / N = DK_1^4 K_2^2 p_A^{(2)}; \\ p_{AC}^{(1O_2)} &= \frac{1}{N} \sum_{i=0}^2 iN_{O_2}^i = DK_1 K_2^4 p_A^{(1)} \exp \frac{\alpha}{\kappa\Theta}; & p_{AC}^{(1O_2)^0} &= 2p_A^{(1)} N_C^{(O_2)} / N = DK_1^2 K_2^4 p_A^{(1)}; \\ p_{AC}^{(2O_2)} &= \frac{1}{2N} \sum_{j=0}^4 jN_{O_2}^j = DK_1^2 K_2^3 p_A^{(2)} \exp \frac{\alpha}{\kappa\Theta}; & p_{AC}^{(2O_2)^0} &= 2p_A^{(2)} N_C^{(O_2)} / N = DK_1^2 K_2^4 p_A^{(2)}; \\ p_{AC}^{(1T)} &= \frac{1}{4N} \sum_{i=0}^2 iN_T^i = DK_1' K_2'^2 p_A^{(1)} \exp \frac{\alpha'}{\kappa\Theta}; & p_{AC}^{(1T)^0} &= \frac{1}{2} p_A^{(1)} N_C^{(T)} / N = DK_1'^2 K_2'^2 p_A^{(1)}; \\ p_{AC}^{(2T)} &= \frac{1}{4N} \sum_{j=0}^2 jN_T^j = DK_1'^2 K_2' p_A^{(2)} \exp \frac{\alpha'}{\kappa\Theta}; & p_{AC}^{(2T)^0} &= \frac{1}{2} p_A^{(2)} N_C^{(T)} / N = DK_1'^2 K_2'^2 p_A^{(2)}. \end{aligned} \quad (24)$$

The differences in these possibilities determine the correlation parameters. Similarly, correlation parameters can be found for pairs of B, C atoms. Using calculations, we find

$$\begin{aligned}
 \varepsilon^{(1O_1)} = \varepsilon_{AC}^{(1O_1)} = -\varepsilon_{BC}^{(1O_1)} &= DK_1^3 K_2^2 p_A^{(1)} p_B^{(1)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right); \\
 \varepsilon^{(2O_1)} = \varepsilon_{AC}^{(2O_1)} = -\varepsilon_{BC}^{(2O_1)} &= DK_1^4 K_2 p_A^{(2)} p_B^{(2)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right); \\
 \varepsilon^{(1O_2)} = \varepsilon_{AC}^{(1O_2)} = -\varepsilon_{BC}^{(1O_2)} &= DK_1 K_2^4 p_A^{(1)} p_B^{(1)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right); \\
 \varepsilon^{(2O_2)} = \varepsilon_{AC}^{(2O_2)} = -\varepsilon_{BC}^{(2O_2)} &= DK_1^2 K_2^3 p_A^{(2)} p_B^{(2)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right); \\
 \varepsilon^{(1T)} = \varepsilon_{AC}^{(1T)} = -\varepsilon_{BC}^{(1T)} &= DK_1' K_2'^2 p_A^{(1)} p_B^{(1)} \left(\exp \frac{\alpha'}{\kappa\Theta} - \exp \frac{\beta'}{\kappa\Theta} \right); \\
 \varepsilon^{(2T)} = \varepsilon_{AC}^{(2T)} = -\varepsilon_{BC}^{(2T)} &= DK_1'^2 K_2' p_A^{(2)} p_B^{(2)} \left(\exp \frac{\alpha'}{\kappa\Theta} - \exp \frac{\beta'}{\kappa\Theta} \right).
 \end{aligned} \tag{25}$$

The obtained formulas, taking into account (22), (17) and (15), determine the dependence of the correlation parameters on the composition of the alloy, temperature, and the degree of long-range order, the knowledge of which can allow determining the formation of short-range ordering or stratification of atoms in the alloy. The correlation parameters for octapores and tetrapores can be of different signs, for example, when $\alpha > \beta$ and $\alpha' < \beta'$. This means that C atoms will primarily concentrate in the octahedral interstices. For a disordered alloy

$$(\eta = 0, K = K_1 = K_2 =$$

$$= a \exp \frac{\alpha}{\kappa\Theta} + b \exp \frac{\beta}{\kappa\Theta},$$

$$K' = K_1' = K_2' = a \exp \frac{\alpha'}{\kappa\Theta} + b \exp \frac{\beta'}{\kappa\Theta})$$

only two correlation parameters are preserved for pores O and T:

$$\varepsilon^{(O)} = 3abcK^5 \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right) / (K^6 + 2K'^4);$$

$$\varepsilon^{(T)} = 3abcK'^5 \left(\exp \frac{\alpha'}{\kappa\Theta} - \exp \frac{\beta'}{\kappa\Theta} \right) / (K^6 + 2K'^4).$$

(26)

The dependence of the $\varepsilon^{(O)}$ and $\varepsilon^{(T)}$ values on the composition is extreme and asymmetric. The maximum of this dependence is manifested in the composition

$$a_* = \left(\exp \frac{\alpha - \beta}{2\kappa\Theta} + 1 \right)^{-1}.$$

For $\varepsilon^{(O)}$ and at $a_* = \left(\exp \frac{\alpha' - \beta'}{\kappa\Theta} + 1 \right)^{-1}$ for $\varepsilon^{(T)}$. As the temperature increases, the asymmetry of the concentration dependence decreases, and at very high temperatures the value of a_* is close to the stoichiometric composition of ($a_* \approx 1/2$). At high temperatures, formulas (26) are simplified

$$\varepsilon^{(O)} = abc \frac{\alpha - \beta}{\kappa\Theta}; \quad \varepsilon^{(T)} = abc \frac{\alpha' - \beta'}{\kappa\Theta}. \tag{27}$$

Finally, we will write down the formulas for the correlation parameters in the case of distribution of atoms only in octapores or only in tetrapores. In the first case $c = Nc/N$, $D = 2c [K_1 K_2 (K_1^2 + K_2^2)]^{-1}$ and

$$\varepsilon^{(1O_1)} = 2cp_A^{(1)} p_B^{(1)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right) K_1 / (K_1^2 + K_2^2);$$

$$\varepsilon^{(2O_1)} = 2cp_A^{(2)} p_B^{(2)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right) K_1^2 / K_2 (K_1^2 + K_2^2);$$

$$\begin{aligned}\varepsilon^{(10_2)} &= 2cp_A^{(1)} p_B^{(1)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right) K_2^2 / K_1 (K_1^2 + K_2^2); \\ \varepsilon^{(20_2)} &= 2cp_A^{(2)} p_B^{(2)} \left(\exp \frac{\alpha}{\kappa\Theta} - \exp \frac{\beta}{\kappa\Theta} \right) K_2 / (K_1^2 + K_2^2); \\ &\quad (28)\end{aligned}$$

in the second $c = Nc/2N$, $D = c(K_1' + K_2')^{-2}$ and

$$\begin{aligned}\varepsilon^{(1T)} &= cp_A^{(1)} p_B^{(1)} \left(\exp \frac{\alpha'}{\kappa\Theta} - \exp \frac{\beta'}{\kappa\Theta} \right) / K_1', \\ \varepsilon^{(2T)} &= cp_A^{(2)} p_B^{(2)} \left(\exp \frac{\alpha'}{\kappa\Theta} - \exp \frac{\beta'}{\kappa\Theta} \right) / K_2'. \\ &\quad (29)\end{aligned}$$

CONCLUSIONS

Knowing the correlation parameters (25) or (29) and (28) allows one to estimate many physical characteristics of alloys. If the

correlation parameters are known from experiments, the obtained formulas allow one determining the energy parameters of alloys, which has a high scientific value.

Атоми впровадження у кристалічній гексагональній структурі

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В рамках роботи розглянуто гексагональну структуру металів типу В19 як сорбентів водню. Розглядаються кристалічні ґатки, де в міжвузлі металу впроваджуються атоми домішок (водень). Для цього у роботі наведено зображення самої структури В19. В роботі вивчено розчинність водню в кристалічній структурі металів типу В19, використовуючи метод конфігурацій, а також знайдено в заміщенні вузлів і міжвузлів залежність від складу сплаву та температури. Також розглянуто ступінь далекого порядку у вузлах та визначено параметри кореляції у заміщенні. Наведено графічний вигляд впливу атомного порядку на розчинність домішок. Розраховані дані, які отримані у роботі, збігаються з експериментальними даними інших досліджень, а отримані формули розрахунків дозволяють визначити енергетичні параметри сплавів, що мають певну наукову цінність. Запропонована система враховує лише атомну взаємодію та абсорбцію (розчинення), дифузії атомів впровадження в об'єм кристалічної структури, тому можна прогнозувати введення лише атома водню). Таким чином, отримані в роботі результати щодо параметрів кореляції при розподілі атомів лише в октапорах або лише в тетрапорах дозволяють глибше вивчати фізичні характеристики сплавів типу В19 і зрозуміти процеси сорбції водню робочими тілами для накопичувачів водню.

Ключові слова: водень, метал, сплави, розчинність, введення домішок, кореляційні параметри, домішки заміщення, структура В19

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